

Polarizers and Retarders

Last time, discussed basics of polarization

Linear, circular, elliptical states

Describe by polarization vector \hat{j}

Today:

Describe elements used to manipulate polarization

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Outline:

- Polarizers
 - Reflection, scattering, dichroism
 - Calculations with polarizers
- Birefringence
- Retarders

Next time: Jones calculus

- powerful tool for doing calculations
- will be helpful for hw

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Polarizers (Hecht 8.2)

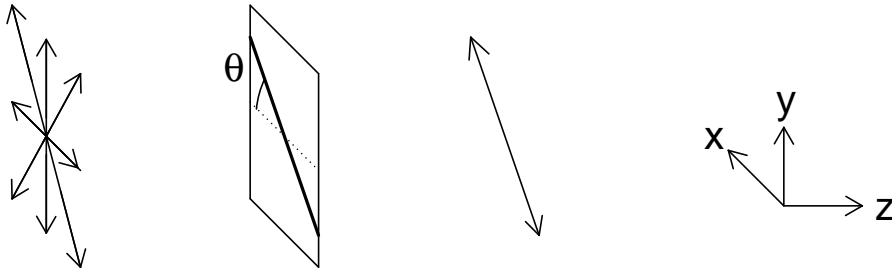
Most natural light sources are unpolarized

Obtain polarized light with *polarizer*

= “filter” passing only one polarization state

Usually transmit linear polarization

Plane of polarization given by *transmission axis*



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Ideal polarizer:

Transmission for $\hat{j} \parallel \text{axis} = 1$

Transmission for $\hat{j} \perp \text{axis} = 0$

If axis at angle θ , write

$$\mathbf{a} = \cos \theta \hat{\mathbf{x}} + \sin \theta \hat{\mathbf{y}}$$

If incident light has polarization \hat{j} :

transmit component of $\hat{j} \parallel \mathbf{a} : \hat{j}^* \cdot \mathbf{a}$

So
$$T = |\hat{j}^* \cdot \mathbf{a}|^2$$

If \hat{j} linearly polarized $\hat{j} = \cos \alpha \hat{\mathbf{x}} + \sin \alpha \hat{\mathbf{y}}$

Then
$$\begin{aligned} \hat{j}^* \cdot \mathbf{a} &= \hat{j} \cdot \mathbf{a} = \cos \theta \cos \alpha + \sin \theta \sin \alpha \\ &= \cos(\theta - \alpha) \end{aligned}$$

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Gives *Malus's Law*:

For linear polarization incident on polarizer,

$$I_{\text{out}} = I_{\text{in}} \cos^2(\theta - \alpha)$$

$\theta - \alpha =$ angle difference between transmission axis and incident plane of polarization

But $T = |\hat{j}^* \cdot \mathbf{a}|^2$ is more general

works for any incident polarization state

Question: Could \mathbf{a} be complex? What would it mean if it were?

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Example:

If $\hat{j}_{\text{inc}} = \hat{\mathbf{e}}_{\mathcal{R}} = \frac{\hat{\mathbf{x}} - i\hat{\mathbf{y}}}{\sqrt{2}}$, what is transmission through linear polarizer at angle θ ?

$$\text{Have } \hat{j}^* \cdot \mathbf{a} = \frac{\cos \theta + i \sin \theta}{\sqrt{2}} = \frac{1}{\sqrt{2}} e^{i\theta}$$

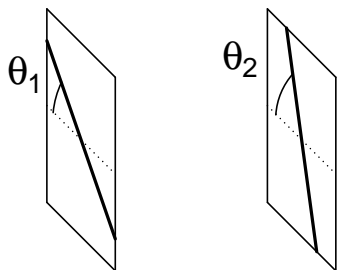
$$\text{So } T = \frac{1}{2} |e^{i\theta}|^2 = \frac{1}{2} \text{ independent of } \theta$$

Makes sense, circ polarization symmetric in θ

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Note, light exiting ideal polarizer has $\hat{j}_{\text{out}} = \mathbf{a}$

If two polarizers: first at θ_1 , second at θ_2



Output of first = polarized along θ_1

Transmission of second = $\cos^2(\theta_2 - \theta_1)$

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Real polarizers aren't perfect:

- Transmission for $\hat{j} \parallel \mathbf{a} = T_0 < 1$
(loss)
- Transmission for $\hat{j} \perp \mathbf{a} = \epsilon > 0$
(leakage)
- Output light not exactly polarized along \mathbf{a}
(rarely specified)

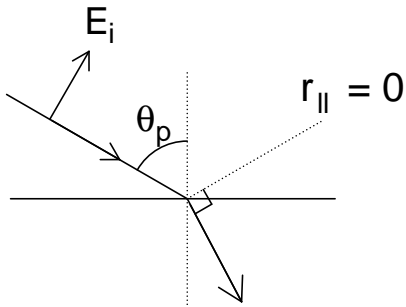
Values depend on type of polarizer

Discuss types of polarizers

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Constructing Polarizers (Hecht 8.3–8.6)

Already know one way to polarize light:
use Brewster's angle



When TM polarized light incident at angle
 $\theta_p = \tan^{-1}(n_t/n_i)$

Get $r_{\parallel} = 0$

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Two ways to make polarizer:

- Use reflected light: get \perp component

Then loss is very high:

- glass, get $R_{\perp} \approx 0.2 \rightarrow$ lose 80%

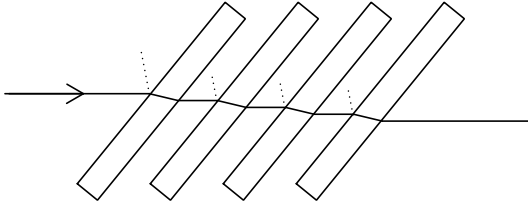
Also, leakage is fairly high:

- hard to control angle accurately

- Better: use transmitted light
and many surfaces

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Pile of plates polarizer:



Each surface transmits all of I_{\parallel}
and fraction T_{\perp} of I_{\perp}
for glass, $T_{\perp} \approx 0.8$

For N plates, total \perp transmission = $T_{\perp\text{tot}} = T_{\perp}^{2N}$

Say glass plates, $N = 10$: $T_{\perp\text{tot}} = 0.01$

Typically get total $T_{\parallel\text{tot}} = 0.5$

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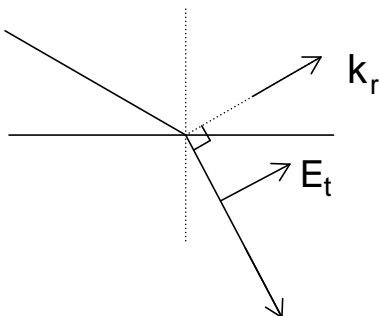
Pile of plates simple and robust

But often awkward to use:

thick, requires collimated light

Based on scattering properties:

Recall Brewster angle when $\mathbf{k}_{\text{ref}} \parallel \mathbf{E}_{\text{trans}}$

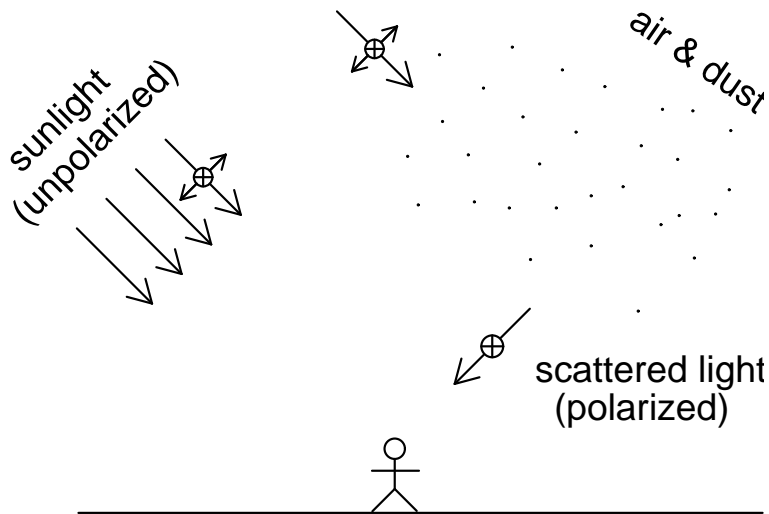


Atoms in glass can't radiate $\parallel \mathbf{E}$
(Charges radiate \perp acceleration)

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Scattered light is generally polarized

Example: light from sky



Not typically useful as polarizer

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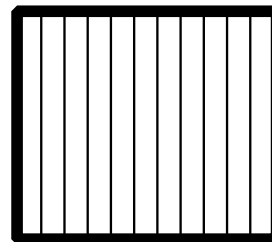
Dichroism (Hecht 8.3)

Dichroism = selective absorption of one (linear) polarization

Clearly useful for polarizers

Example: microwave polarizer

Array of parallel wires
spacing $\ll \lambda$



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\mathbf{E} aligned with wires: drive current
resistance \rightarrow power dissipation
 \rightarrow absorption

$\mathbf{E} \perp$ wires: little current, no absorption

Acts as a polarizer: transmits only $\mathbf{E} \perp$ wires

Watch out: graphically, want to picture vertical \mathbf{E}
“squeezing” through slots

Actual effect is just the opposite!

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Optical version: wires \rightarrow long polymer chains
Embed in clear plastic
Stretch plastic to align chains

Material called *polaroid*

Most common polarizer

Great for demos!

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Characteristics of polaroid:

- Somewhat lossy: $T_0 \approx 0.7$
- Low leakage $\epsilon \approx 10^{-3}$
- Work best for visible light
- Cheap: \$1 for 5 cm square

Important restriction: limited to low power
(plastic can melt)

Don't use with higher intensity laser beams
 $\max I \approx 1 \text{ W/cm}^2$

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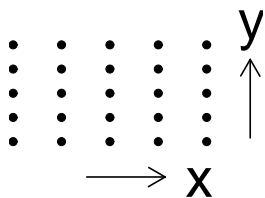
Birefringence (Hecht 8.4)

Best polarizers based on *birefringence*

- Property of certain crystals

Generally, different directions not equivalent

Possible crystal lattice:



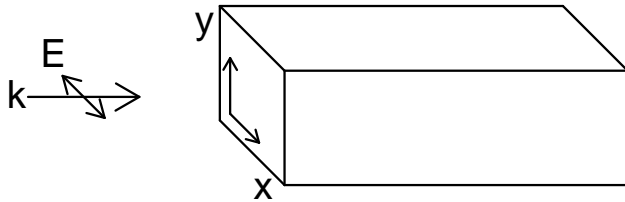
x and y axes different

Note x and y = symmetry axes of crystal

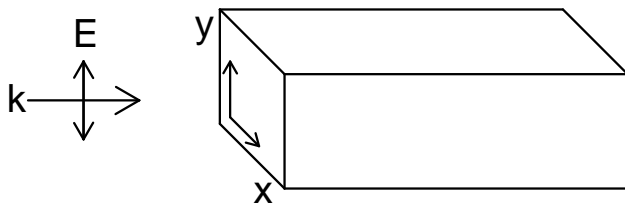
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In asymmetric crystal, index of refraction n depends on direction of \mathbf{E}

If \mathbf{E} along x then have $n = n_x$:



If \mathbf{E} along y then $n = n_y$:



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All crystals have three basic symmetry axes for now, label x , y and z

Call n_x , n_y , $n_z =$ *principle indices of refraction*

Three different kinds of crystals:

- isotropic: $n_x = n_y = n_z$
- not birefringent
- uniaxial: $n_x = n_y \neq n_z$
- z axis special: called optic axis
- biaxial: $n_x \neq n_y \neq n_z$
- optical properties complicated

Question: Can a liquid be birefringent?

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Focus on uniaxial:

Symmetry like a cylinder: x and y interchangeable

Terminology: call $n_x, n_y = n_o$
ordinary index

Call $n_z = n_e$: extraordinary index

Common optical materials:

Calcite: $n_o = 1.658, n_e = 1.486$

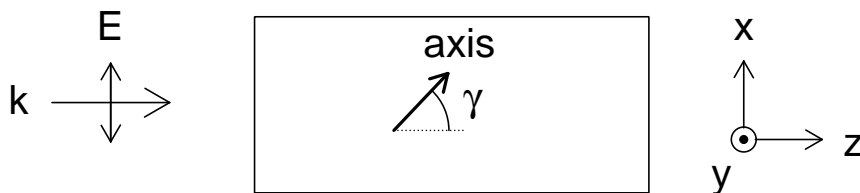
Quartz: $n_o = 1.544, n_e = 1.553$

Other examples: ice, mica, sapphire, LiNbO_3

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What happens if \mathbf{k} is not along a crystal axis?

Example:



Light propagates along z

\mathbf{E} along x

optic axis at angle γ in xz -plane

Question: What is index if \mathbf{E} along y ?

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For \mathbf{E} along x , get effective index n_{eff} :

$$\frac{1}{n_{\text{eff}}^2} = \frac{\cos^2 \gamma}{n_o^2} + \frac{\sin^2 \gamma}{n_e^2}$$

If $\gamma = 0$, $n_{\text{eff}} = n_o$

if $\gamma = 90^\circ$, $n_{\text{eff}} = n_e$

Otherwise n_{eff} between n_o and n_e

Derivation a bit hard, won't go through

See Klein and Furtak §9.4

Probably cover in Phys 532

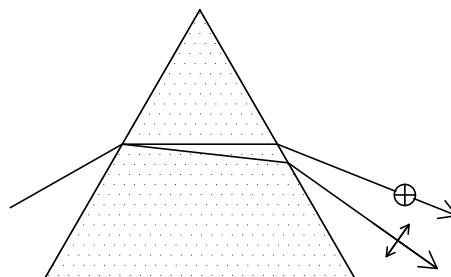
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Upshot:

In birefringent materials, n depends on polarization

Simple polarizer:

Calcite prism, axis \perp to page



\perp and \parallel polarizations have different n 's

Deflected by different amounts

Separate outputs with lens or free propagation

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Example of a *polarizing beam splitter*

= polarizer with two outputs
one for each state

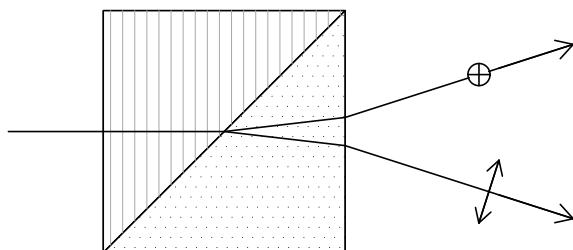
But not a good design:

- Deflection depends on λ
- Significant reflection from surfaces
- Large common deflection inconvenient

Improve by putting two prisms together

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Wollaston prism:



Typical angular separation = 15-20°

Good performance:

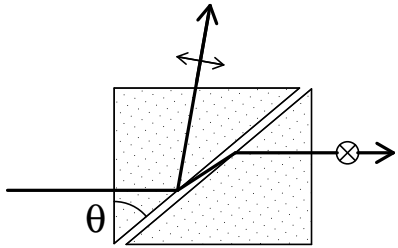
- Loss \approx 10%, or 1% if AR coated
- Leakage $\sim 10^{-5}$
- Works at high power

Several other designs, see optics catalogs

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Another good design: Glan-Thompson

Uses total internal reflection



Again calcite, with optical axis \perp page

Choose prism angle so that $n_e \sin \theta < 1 < n_o \sin \theta$

$\theta = 40^\circ$ works

Then o -light is TIR, e -light is transmitted

(Gap is too big for frustrated TIR)

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Performance similar to Wollaston

- low loss, low leakage
- high power capacity

Advantage: larger beam separation

no deviation of e beam

Wollaston and Glan-Thompson expensive

\$300-\$500 or more

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Retarders (Hecht 8.7)

Use polarizers to make linear polarized light

What about circular or elliptical?

Use *retarder*

Most common retarder = wave plate

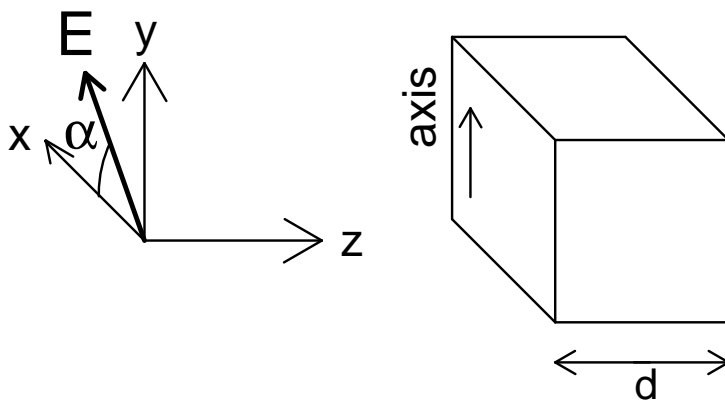
Again based on birefringence

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Suppose linear polarized light, angle α

Incident on uniaxial crystal with axis vertical

Crystal thickness d



Coordinates as shown: $z = 0$ at front of crystal

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Incident wave has $\hat{j} = \cos \alpha \hat{x} + \sin \alpha \hat{y}$

$$\mathbf{E}_{\text{inc}} = E_0 \hat{j} e^{i(\mathbf{k} \cdot \mathbf{r} - \omega t)}$$

In crystal $k \rightarrow nk_0$

different for E_x and E_y components

So

$$\mathbf{E}_{\text{crystal}} = E_0 \left(\cos \alpha e^{in_0 k_0 z} \hat{x} + \sin \alpha e^{in_e k_0 z} \hat{y} \right) e^{-i\omega t}$$

At output $z = d$:

$$\begin{aligned} \mathbf{E}_d &= E_0 \left(\cos \alpha e^{in_0 k_0 d} \hat{x} + \sin \alpha e^{in_e k_0 d} \hat{y} \right) e^{-i\omega t} \\ &= E_0 e^{in_0 k_0 d} \left[\cos \alpha \hat{x} + \sin \alpha e^{i(n_e - n_0) k_0 d} \hat{y} \right] e^{-i\omega t} \end{aligned}$$

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Define $\hat{j}_{\text{out}} = \cos \alpha \hat{x} + \sin \alpha e^{i(n_e - n_0) k_0 d} \hat{y}$

Then after crystal, have

$$\begin{aligned} E(z, t) &= E_0 e^{in_0 k_0 d} \hat{j}_{\text{out}} e^{i[k(z-d) - \omega t]} \\ &= E_0 e^{i(n_0 - 1) k_0 d} \hat{j}_{\text{out}} e^{i(kz - \omega t)} \\ &= E'_0 \hat{j}_{\text{out}} e^{i(kz - \omega t)} \end{aligned}$$

Get plane wave out with

$$\hat{j} = \cos \alpha \hat{x} + \sin \alpha e^{i\varepsilon} \hat{y}$$

with $\boxed{\varepsilon = (n_e - n_0) k_0 d} \equiv \text{retardance}$

Set d to achieve desired ε value

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By adjusting α and ε ,
make arbitrary polarization state

Example: $kd(n_e - n_o) = \pi/2$

Then $d(n_e - n_o) = \lambda/4$: call *quarter-wave plate*

$$\begin{aligned}\hat{j}_{\text{out}} &= \cos \alpha \hat{x} + e^{i\pi/2} \sin \alpha \hat{y} \\ &= \cos \alpha \hat{x} + i \sin \alpha \hat{y}\end{aligned}$$

$$\text{For } \alpha = \pm 45^\circ, \hat{j}_{\text{out}} = \frac{\hat{x} \pm i\hat{y}}{\sqrt{2}}$$

Make LHC and RHC polarizations

Main use of quarter-wave plate:
convert linear to circular polarization

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Other common configuration: $\varepsilon = \pi$

Then $d(n_e - n_o) = \lambda/2$: *half-wave plate*

Have $e^{i\pi} = -1$ so

$$\hat{j}_{\text{out}} = \cos \alpha \hat{x} - \sin \alpha \hat{y}$$

Changes polarization angle $\alpha \rightarrow -\alpha$

Suppose $\alpha_{\text{in}} = 45^\circ$

Then $\alpha_{\text{out}} = -45^\circ$:

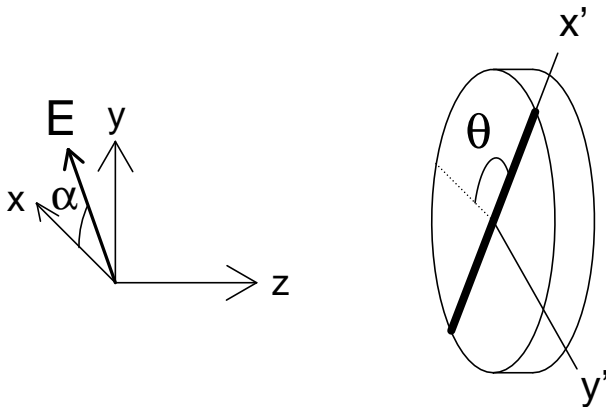
Rotated by 90° : orthogonal to input

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Use half-wave plate by rotating it
how to calculate effect?

⇒ need to express input in crystal basis

Define x' = axis of waveplate



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Then

$$\hat{x}' = \cos \theta \hat{x} + \sin \theta \hat{y}$$

$$\hat{y}' = \cos \theta \hat{y} - \sin \theta \hat{x}$$

and $\hat{j} = \cos \alpha \hat{x} + \sin \alpha \hat{y}$

Calculate $j_{x'} = \hat{j} \cdot \hat{x}'$

$$= \cos \alpha \cos \theta - \sin \alpha \sin \theta = \cos(\alpha - \theta)$$

and $j_{y'} = \hat{j} \cdot \hat{y}'$

$$= -\cos \alpha \sin \theta + \sin \alpha \cos \theta = \sin(\alpha - \theta)$$

Or $\hat{j} = \cos \alpha' \hat{x}' + \sin \alpha' \hat{y}'$ for $\alpha' = \alpha - \theta$

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Effect of half wave plate is $\alpha' \rightarrow -\alpha'$

So $\alpha_{\text{out}} - \theta = -(\alpha_{\text{in}} - \theta)$

$$\alpha_{\text{out}} = 2\theta - \alpha_{\text{in}}$$

As θ adjusted, output polarization rotates by 2θ

Main use of half-wave plate:
rotate linear polarization by arbitrary angle

Question: What happens when $\theta = \alpha_{\text{in}}$? What is physically happening in this situation?

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One problem: waveplates very thin

Quarter wave plate: $d = \lambda/4(n_e - n_o) \sim \lambda$

Often make $\varepsilon = \pi/4 + 2\pi m$ for integer m :
get same effect

Called *multiple order waveplate*
typical $m \approx 10$

Most common waveplate material: quartz
cost \$200 for 1-cm diameter plate

Cheaper: plastic (\$5 for 5 cm square)
- ε less accurate
- distorts laser beams

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Terminology:

Fast axis: axis of wave plate with lower n

Slow axis: axis of wave plate with higher n

Doesn't really matter which is optical axis

depends on whether $n_o > n_e$ ("negative" crystal)

or $n_o < n_e$ ("positive" crystal)

Other ways to make retarders (Hecht pg 356-357):

- Fresnel rhomb: use phase shift from TIR

- Babinet-Soliel compensator:

waveplate with variable thickness

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Summary:

- Polarizers transmit one polarization

$$T = T_0 |\hat{j}^* \cdot \mathbf{a}|^2$$

- Most polarizers dichroic or birefringent

Birefringent better, more \$

- Birefringence: n depends on \hat{j}

- Uniaxial crystal: one special direction

- Retarders use birefringence

- Quarter-wave plate: make circ polarization

- Half-wave plate: rotate linear polarization

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