

Fresnel Relations

Last time, starting looking at how light propagates across boundaries.

Scattering idea \rightarrow law of reflection, Snell's law
Generalized to Fermat's principle

Important question:

How much light will be reflected vs transmitted?

Answer today using Maxwell equations

1

Outline:

- Boundary conditions for \mathbf{E} and \mathbf{B}
- Fresnel equations
- Brewster's angle
- Reflectance and transmittance

Everything today from Hecht 4.6

Next time: when the Fresnel equations become complex

2

Boundary Conditions

Maxwell equations in medium:

$$\begin{aligned}\epsilon_0 \nabla \cdot \mathbf{E} &= -\nabla \cdot \mathbf{P} & \nabla \cdot \mathbf{B} &= 0 \\ \nabla \times \mathbf{B} &= \mu_0 \frac{\partial \mathbf{P}}{\partial t} + \epsilon_0 \mu_0 \frac{\partial \mathbf{E}}{\partial t} & \nabla \times \mathbf{E} &= -\frac{\partial \mathbf{B}}{\partial t}\end{aligned}$$

\mathbf{P} = macroscopic polarization = $\epsilon_0 \chi \mathbf{E}$

Now consider $\chi = \chi(\mathbf{r})$

Rewrite:

$$\begin{aligned}\epsilon_0 \nabla \cdot [(1 + \chi)\mathbf{E}] &= 0 & \nabla \cdot \mathbf{B} &= 0 \\ \nabla \times \mathbf{B} &= \epsilon_0 \mu_0 \frac{\partial}{\partial t} [(1 + \chi)\mathbf{E}] & \nabla \times \mathbf{E} &= -\frac{\partial \mathbf{B}}{\partial t}\end{aligned}$$

3

Recall $\epsilon_0(1 + \chi) \equiv \epsilon$, electric permittivity

Convenient to define $\mathbf{D} = \epsilon \mathbf{E}$

“Electric displacement” (units C/m²)

Then have

$$\begin{aligned}\nabla \cdot \mathbf{D} &= 0 & \nabla \cdot \mathbf{B} &= 0 \\ \nabla \times \mathbf{B} &= \mu_0 \frac{\partial \mathbf{D}}{\partial t} & \nabla \times \mathbf{E} &= -\frac{\partial \mathbf{B}}{\partial t}\end{aligned}$$

“Hides” charges of medium, even when crossing boundaries

Works for conductors too, if $\epsilon \rightarrow$ complex

4

Know how wave propagates in uniform medium

Don't know how to relate \mathbf{D} , \mathbf{E} and \mathbf{B} on opposite sides of boundary

Easiest to go back to integral form:

$$\text{If } \nabla \cdot \mathbf{D} = 0, \text{ then } \oiint \mathbf{D} \cdot d\mathbf{S} = 0$$

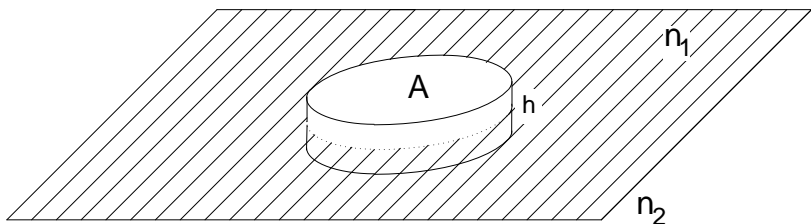
See what this says about boundary

5

Make little pillbox surface on boundary:

area A small but nonzero

height $h \rightarrow 0$



$$\text{Then } \oiint \mathbf{D} \cdot d\mathbf{S} \rightarrow A(D_{1\perp} - D_{2\perp}) = 0$$

where D_{\perp} = component of \mathbf{D} normal to boundary

So D_{\perp} is continuous across boundary

6

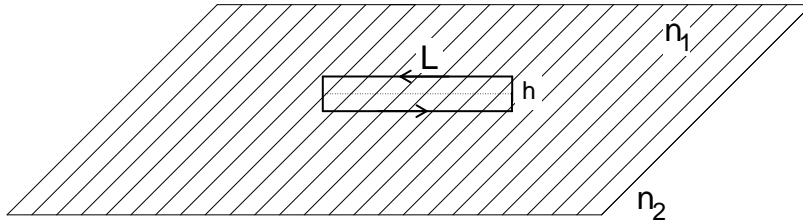
Also have

$$\oint \mathbf{E} \cdot d\mathbf{l} = - \iint \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{S}$$

Make little loop normal to boundary

length L small

height $h \rightarrow 0$



7

Then $\oint \mathbf{E} \cdot d\mathbf{l} \rightarrow L(E_{1\parallel} - E_{2\parallel})$

E_{\parallel} = component of \mathbf{E} parallel to boundary

And

$$\begin{aligned} \iint \frac{\partial \mathbf{B}}{\partial t} \cdot d\mathbf{S} &\rightarrow \frac{Lh}{2} \left(\frac{\partial B_{1\parallel}}{\partial t} + \frac{\partial B_{2\parallel}}{\partial t} \right) \\ &= 0 \quad \text{for } h \rightarrow 0 \end{aligned}$$

So \mathbf{E}_{\parallel} is continuous across boundary

8

Similarly, from

$$\oiint \mathbf{B} \cdot d\mathbf{S} = 0 \text{ and } \oint \mathbf{B} \cdot d\mathbf{l} = \mu_0 \iint \frac{\partial \mathbf{D}}{\partial t} \cdot d\mathbf{S}$$

show that B_{\perp} and B_{\parallel} are continuous

So \mathbf{B} is same on either side of boundary

Note: only true for nonmagnetic materials
(normal in optics)

Hecht gives general formulas

9

Apply continuity conditions to boundary $n_i \rightarrow n_t$

Three fields:

$$\text{Incident } \mathbf{E}_i = \mathbf{E}_{i0} e^{i(\mathbf{k}_i \cdot \mathbf{r} - \omega t)}$$

$$\text{Reflected } \mathbf{E}_r = \mathbf{E}_{r0} e^{i(\mathbf{k}_r \cdot \mathbf{r} - \omega t)}$$

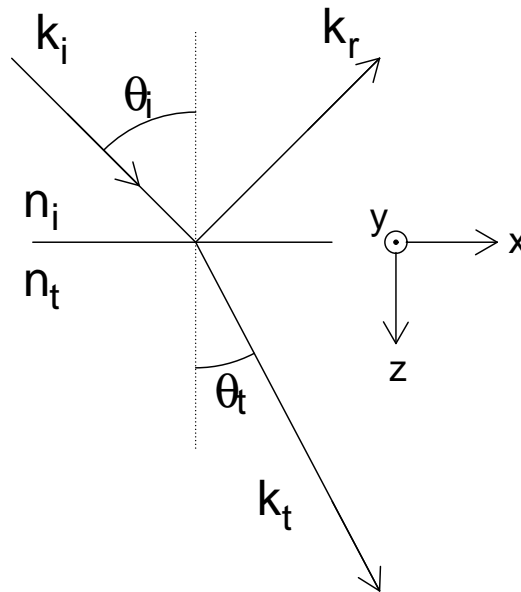
$$\text{Transmitted } \mathbf{E}_t = \mathbf{E}_{t0} e^{i(\mathbf{k}_t \cdot \mathbf{r} - \omega t)}$$

Here $\mathbf{k}_i = n_i \frac{\omega}{c} \hat{\mathbf{k}}_i$ etc. Also have $\mathbf{B} = \frac{n}{c} \hat{\mathbf{k}} \times \mathbf{E}$ for each

Want to determine \mathbf{E}_r and \mathbf{E}_t if given \mathbf{E}_i

10

Set up coordinates
so $k_y = 0$ always



At $z = 0$, have:

$$\mathbf{B}_i + \mathbf{B}_r = \mathbf{B}_t$$

$$E_{ix} + E_{rx} = E_{tx}$$

$$E_{iy} + E_{ry} = E_{ty}$$

$$n_i^2 E_{iz} + n_i^2 E_{rz} = n_t^2 E_{tz}$$

Question: Wait, where did those n^2 's come from?

11

E_x equation says

$$E_{i0x} e^{i(k_{ix}x - \omega t)} + E_{r0x} e^{i(k_{rx}x - \omega t)} = E_{t0x} e^{i(k_{tx}x - \omega t)}$$

for all x

Only possible if $k_{ix} = k_{rx} = k_{tx}$

Implies $\sin \theta_i = \sin \theta_r$ and $n_i \sin \theta_i = n_t \sin \theta_t$

- Gives law of reflection, Snell's law

So x dependence drops out, leaves equations for amplitudes $\mathbf{E}_0, \mathbf{B}_0$

example: $E_{i0x} + E_{r0x} = E_{t0x}$

12

Easiest to separate two cases:

Case I: $E_{i0x} = 0$

Then all E_x components = 0

So \mathbf{E}_0 's are \perp to plane of incidence

Called "s-polarized" or "TE-polarized"

Case II: $E_{i0y} = 0$

Then all E_y components = 0

So \mathbf{E}_0 's are in plane of incidence

Called "p-polarized" or "TM-polarized"

Can write general wave as superposition of these

13

Case I: $\mathbf{E} \propto \hat{y}$

So \mathbf{B} in xz -plane

Continuity:

$E_{i0y} = E_{i0}$ etc,

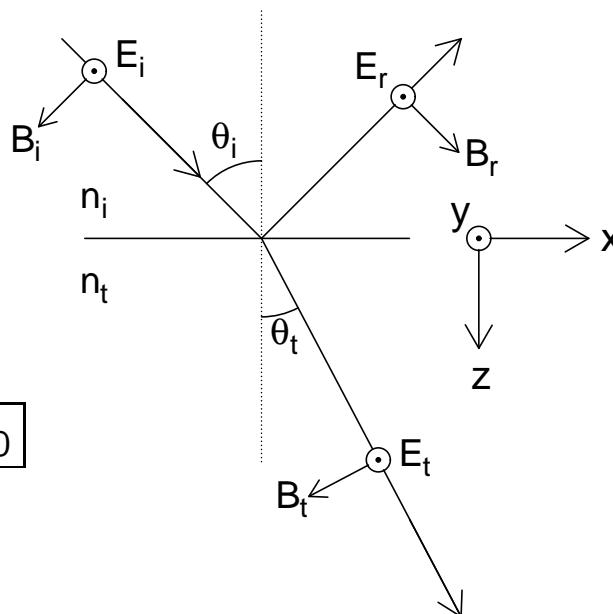
$$\text{so } \boxed{E_{i0} + E_{r0} = E_{t0}}$$

For \mathbf{B} :

$$B_{i0x} = -B_{i0} \cos \theta_i$$

$$B_{r0x} = B_{r0} \cos \theta_i$$

$$B_{t0x} = -B_{t0} \cos \theta_t$$



14

Have $B_{i0x} + B_{r0x} = B_{t0x}$, and

$$B_{i0x} = \frac{n_i}{c} E_{i0} \text{ etc.}$$

so

$$\boxed{-n_i E_{i0} \cos \theta_i + n_i E_{r0} \cos \theta_i = -n_t E_{t0} \cos \theta_t}$$

Two equations, two unknowns E_{r0} and E_{t0}
(B_z equation is redundant)

15

Solve:

$$\begin{aligned} (E_{i0} - E_{r0})n_i \cos \theta_i &= E_{t0}n_t \cos \theta_t \\ &= (E_{i0} + E_{r0})n_t \cos \theta_t \end{aligned}$$

$$E_{i0}(n_i \cos \theta_i - n_t \cos \theta_t) = E_{r0}(n_i \cos \theta_i + n_t \cos \theta_t)$$

Write $E_{r0} = r_{\perp} E_{i0}$ for

$$\boxed{r_{\perp} = \frac{n_i \cos \theta_i - n_t \cos \theta_t}{n_i \cos \theta_i + n_t \cos \theta_t}}$$

r_{\perp} = amplitude reflection coefficient
(for TE polarization)

16

Then get E_{t0} :

$$(E_{i0} - E_{r0})n_i \cos \theta_i = E_{t0}n_t \cos \theta_t$$

$$E_{t0} = \frac{n_i \cos \theta_i}{n_t \cos \theta_t} (1 - r_{\perp}) E_{i0}$$

Define $E_{t0} = t_{\perp} E_{i0}$

$$\begin{aligned} t_{\perp} &= \frac{n_i \cos \theta_i}{n_t \cos \theta_t} (1 - r_{\perp}) \\ &= \frac{n_i \cos \theta_i}{n_t \cos \theta_t} \frac{2n_t \cos \theta_t}{n_i \cos \theta_i + n_t \cos \theta_t} \end{aligned}$$

17

So
$$t_{\perp} = \frac{2n_i \cos \theta_i}{n_i \cos \theta_i + n_t \cos \theta_t}$$

amplitude transmission coefficient
(s-polarization)

This solves case I

Question: What happens to r_{\perp} and t_{\perp} if $n_i = n_t$?

18

Case II:

Now have $\mathbf{B} \perp$ plane

$$B_{i0} + B_{r0} = B_{t0}$$

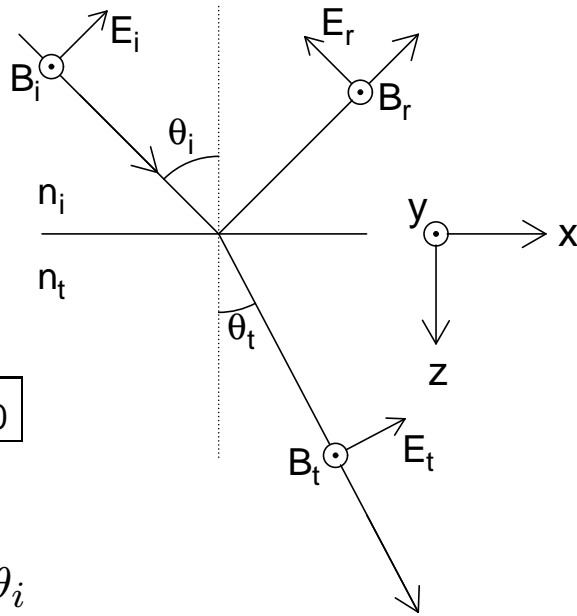
or $n_i E_{i0} + n_i E_{r0} = n_t E_{t0}$

For \mathbf{E} : $E_{i0x} = E_{i0} \cos \theta_i$

$$E_{r0x} = -E_{r0} \cos \theta_i$$

$$E_{t0x} = E_{t0} \cos \theta_t$$

$$E_{i0} \cos \theta_i - E_{r0} \cos \theta_i = E_{t0} \cos \theta_t$$



19

Solve, get $E_{r0} = r_{\parallel} E_{i0}$, $E_{t0} = t_{\parallel} E_{i0}$

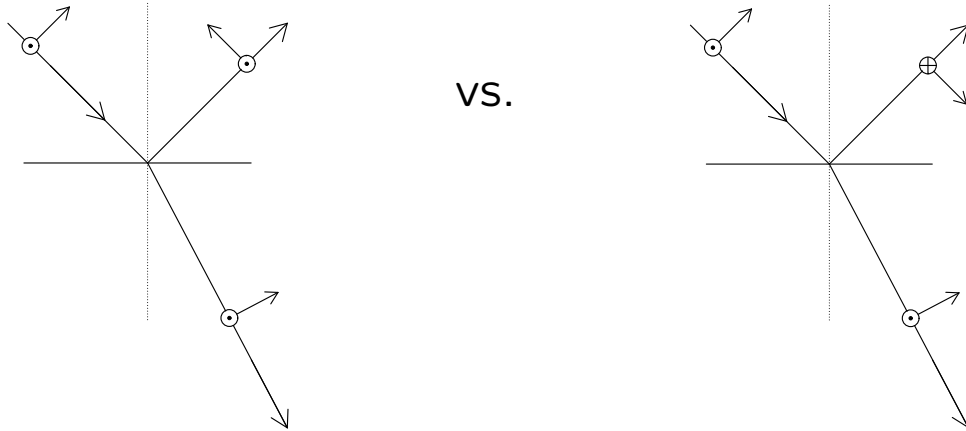
$$r_{\parallel} = \frac{n_t \cos \theta_i - n_i \cos \theta_t}{n_i \cos \theta_t + n_t \cos \theta_i}$$

$$t_{\parallel} = \frac{2n_i \cos \theta_i}{n_i \cos \theta_t + n_t \cos \theta_i}$$

Call r 's, t 's Fresnel coefficients, equations are
Fresnel relations

20

Note: signs depend on picture set up



Gives opposite sign for r 's
 Hecht's set up most common

Question: At normal incidence $r_{\perp} = -r_{\parallel}$. How are the actual directions of \mathbf{E}_{inc} and \mathbf{E}_{ref} related?

21

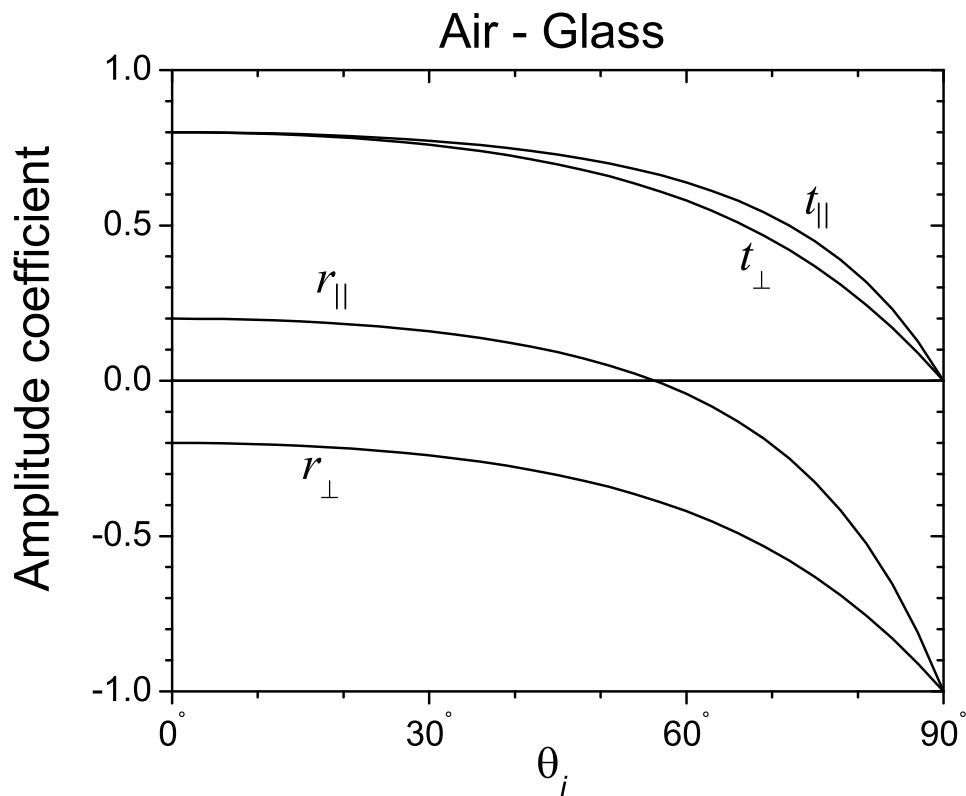
For now consider $n_i < n_t$: "external incidence"
 Plot for air ($n_i = 1$) \rightarrow glass ($n_t = 1.5$)

Need to use Snell's Law to get θ_t

$$\begin{aligned} \cos \theta_t &= \sqrt{1 - \sin^2 \theta_t} \\ &= \sqrt{1 - \frac{n_i^2}{n_t^2} \sin^2 \theta_i} \end{aligned}$$

Question: Do we need to worry about \pm with square root?

22



23

Features:

- $r_{\perp} = -r_{\parallel}$ at $\theta_i = 0$

No physical difference between TE and TM

Picture difference gives minus sign

- $r \rightarrow 1$ as $\theta_i \rightarrow 90^\circ$

Everything reflects at glancing incidence

- $r_{\parallel} \rightarrow 0$ at $\theta_i = \theta_p$

Usually called Brewster's angle

Hecht calls "polarization angle"

Demo!

24

Brewster's angle important for lasers
 best way to minimize reflections

Solve $r_{\parallel} = 0$: $n_t \cos \theta_p = n_i \cos \theta_t$

Get $\sin \theta_p = \frac{n_t}{\sqrt{n_i^2 + n_t^2}}$

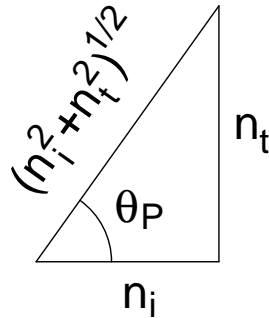
Get some insight:

See $\tan \theta_p = n_t/n_i$

So $n_i \sin \theta_p = n_t \cos \theta_p$

But $n_t \cos \theta_p = n_i \cos \theta_t$

so $\sin \theta_p = \cos \theta_t \Rightarrow \theta_p + \theta_t = 90^\circ$



25

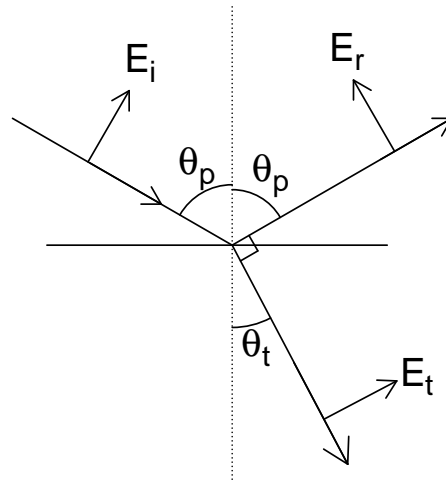
Picture:

Atoms in transmitted medium oscillate along \mathbf{E}_t

Dipole radiation $\rightarrow 0$
 in direction of oscillation

Brewster's angle:

when direction of oscillation = $\hat{\mathbf{k}}_{\text{reflect}}$



For air \rightarrow glass, $\theta_p = 56.3^\circ$

26

Note, r and t are amplitude coefficients:

give E -fields

Usually more interested in transmitted and reflected power P

Define *reflectance* $R = P_{\text{ref}}/P_{\text{inc}}$

transmittance $T = P_{\text{trans}}/P_{\text{inc}}$

Get P from Poynting vector \mathbf{S} :

$$\text{Plane waves: } \mathbf{S} = \frac{n}{2\eta_0} |E_0|^2 \hat{\mathbf{k}}$$

27

Power through area $dA = \mathbf{S} \cdot \hat{\mathbf{u}} dA$

$\hat{\mathbf{u}}$ = normal to surface

here $\hat{\mathbf{k}} \cdot \hat{\mathbf{u}} = \cos \theta$

$$\text{So } P_{\text{inc}} = \frac{n_i}{2\eta_0} |E_{i0}|^2 \cos \theta_i dA$$

$$P_{\text{refl}} = \frac{n_i}{2\eta_0} |E_{j0}|^2 \cos \theta_i dA$$

$$P_{\text{trans}} = \frac{n_t}{2\eta_0} |E_{t0}|^2 \cos \theta_t dA$$

28

Then

$$R = \frac{P_{\text{ref}}}{P_{\text{inc}}} = \frac{|E_{r0}|^2}{|E_{i0}|^2} = |r|^2$$

and

$$T = \frac{P_{\text{trans}}}{P_{\text{inc}}} = \frac{n_t \cos \theta_t |E_{t0}|^2}{n_i \cos \theta_i |E_{i0}|^2} = \frac{n_t \cos \theta_t}{n_i \cos \theta_i} |t|^2$$

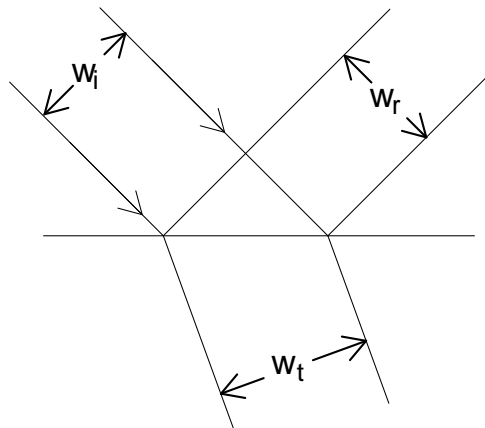
Extra factors in T make sense:

- n accounts for difference in speed
- $\cos \theta$ accounts for difference in area

29

Here $w_t > w_i$

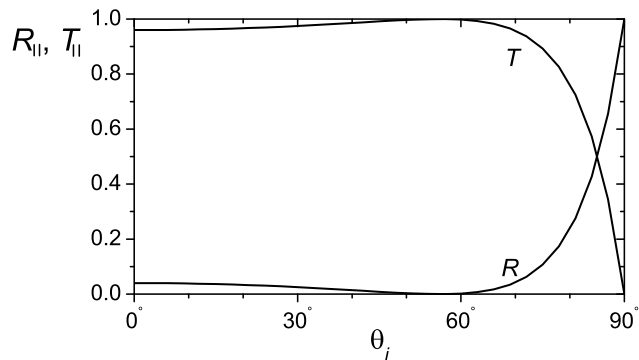
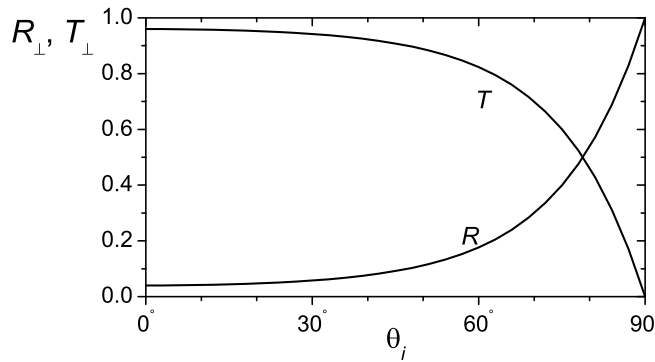
Irradiance decreases even
if all power transmitted



Can show $R + T = 1$ for both \perp and \parallel cases

- Energy conserved (if n is real)

30



31

Summary:

- Maxwell equations give continuity relations
- Fresnel coefficients r , t relate \mathbf{E}_{inc} , \mathbf{E}_{ref} , $\mathbf{E}_{\text{trans}}$
- Two cases \perp (= TE = s) and \parallel (= TM = p) are different
- TM case exhibits Brewster's angle, $r(\theta_p) = 0$
- Fresnel coeffs related to power reflectance R , transmittance T
- Air-glass boundary reflects 4% at $\theta_i = 0$

32