

1. First, solve for mode:

Round trip matrix, starting at flat mirror is

$$M = \begin{bmatrix} 1 & d \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ \frac{2}{R} & 1 \end{bmatrix} \begin{bmatrix} 1 & d \\ 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} 1 & d \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & d \\ \frac{2}{R} & 1 + \frac{2d}{R} \end{bmatrix} = \begin{bmatrix} 1 + \frac{2d}{R} & 2d + \frac{2d^2}{R} \\ \frac{2}{R} & 1 + \frac{2d}{R} \end{bmatrix}$$

$$\text{So } q = \frac{1}{C} \left[\frac{A-D}{2} \pm \sqrt{\left(\frac{A+D}{2}\right)^2 - 1} \right]$$

$$= \pm \frac{R}{2} \sqrt{\left(1 + \frac{2d}{R}\right)^2 - 1} = \pm \frac{R}{2} \sqrt{\frac{4d}{R} + \frac{4d^2}{R^2}}$$

$$= \pm 50 \text{ cm} \sqrt{-2 + 1}$$

$$= \pm 50 \text{ cm} = \dots$$

So focus at back mirror, $z_0 = 50 \text{ cm}$

$$w_0 = \sqrt{\frac{\lambda z_0}{\pi}} = 0.89 \text{ mm}$$

Width at front mirror

$$w(z) = w_0 \sqrt{1 + \frac{z^2}{z_0^2}} = w_0 \sqrt{1 + 1} = \sqrt{2} w_0$$

$$= 1.26 \text{ mm}$$

So, estimate $w \approx 1 \text{ mm}$ in cavity

Second, get medium characteristics.

(2)

density: $P = Nk_B T$

$$P = 1 \text{ atm} = 101325 \text{ N/m}^2$$

$$T = 300 \text{ K}$$

$$\text{So } N_a = \frac{101325 \text{ N/m}^2}{1.38 \times 10^{-23} \text{ J/K} \cdot 300 \text{ K}} = \boxed{2.45 \times 10^{25} \text{ m}^{-3}}$$

linewidth:

$$\text{Reduction } \Delta\nu = \frac{1}{2\pi t_1} = 160 \text{ kHz}$$

$$\text{Collisions } \Delta\nu = \frac{1}{\pi} f_{\text{col}} = 320 \text{ MHz}$$

$$\text{Doppler } \Delta\nu = 2.35 \sqrt{\frac{kT}{M\lambda^2}} = 52 \text{ MHz}$$

$$M = 200 \times 1.66 \times 10^{-27} \text{ kg} = 3.32 \times 10^{-25} \text{ kg}$$

So collisional broadening dominates

Third, find inversion:

For ideal four-level system with

$$\text{no degeneracies, } \Delta N = R(\tau_2 - \tau_1) \approx R\tau_2$$

$$\text{and } R = W_p N_a$$

Since W_p is very small, expect that we can ignore depletion of ground state

$$\text{So } \Delta N = W_p \tau_2 N_a = (10^{-6} \text{ s}^{-1})(10^{-3} \text{ s})(2.45 \times 10^{25} \text{ m}^{-3}) \\ = 2.45 \times 10^{16} \text{ m}^{-3}$$

So small signal gain is

$$g_0 = \frac{\lambda^2}{8\pi\tau_s} g(\nu) \Delta N$$

Assume $\nu \approx \nu_0$, so

$$g(\nu) \rightarrow \frac{2}{\pi\Delta\nu} = \frac{2}{f_{\text{c.o.l}}}$$

$$g_0 = \frac{\lambda^2}{4\pi^2\tau_s\Delta\nu} \Delta N = \frac{\lambda^2\tau_s W_p N_a}{4\pi\tau_s f_{\text{c.o.l}}} = \frac{\lambda^2 W_p N_a}{4\pi f_{\text{c.o.l}}}$$

$$= \frac{(5 \times 10^{-6} \text{ m})^2}{4 \cdot \pi^2 \cdot (10^{-3} \text{ s}) \cdot (320 \text{ MHz})} \cdot 2.45 \times 10^{16} \text{ m}^{-3}$$

$$g_0 = 0.048 \text{ m}^{-1}$$

and $g_0 = 2g_{\text{od}} = 0.048 > \tau$, so above threshold.

$$\text{Also need } I_{\text{set}} = \frac{4\pi^2 h c \tau_s \Delta\nu}{\lambda^3 \tau_s} = \frac{4\pi h c f_{\text{c.o.l}}}{\lambda^3}$$

For ideal four-level system, $\tau_s = \tau_2 = \tau_1$

$$I_s = \frac{4\pi^2 (6.63 \times 10^{-34} \text{ Js}) (3 \times 10^8 \text{ m/s}) (320 \text{ MHz})}{(5 \mu\text{m})^3}$$

$$I_s = 20 \frac{\text{W}}{\text{m}^2}$$

So

$$P_{\text{out}} \approx \pi W^2 I_s T \left(\frac{g_0}{\tau} - 1 \right)$$

$$= \pi (1 \text{ mm})^2 (20 \frac{\text{W}}{\text{m}^2}) (0.02) \left(\frac{0.048}{0.02} - 1 \right)$$

$$P_{\text{out}} = 1.7 \mu\text{W}$$

2.

(4)

Rate equations

$$\frac{dN_2}{dt} = +\omega_p N_0 - \omega_p N_2 - \frac{1}{\tau_2} N_2 = 0$$

$$\frac{dN_1}{dt} = +\frac{1}{\tau_{21}} N_2 - \frac{1}{\tau_1} N_1 = 0 \quad \Rightarrow \quad N_1 = \frac{\tau_1}{\tau_{21}} N_2$$

$$\frac{dN_4}{dt} = +\frac{1}{\tau_{24}} N_2 - \frac{1}{\tau_4} N_4 = 0 \quad \Rightarrow \quad N_4 = \frac{\tau_4}{\tau_{24}} N_2$$

$$N_2 = N_0 \frac{\omega_p}{\omega_p + \frac{1}{\tau_2}} = N_0 \frac{\tau_2 \omega_p}{1 + \tau_2 \omega_p}$$

In terms of N_0 :

$$N_c = N_0 + N_1 + N_2 + N_4$$

$$= N_0 \left(1 + \frac{\tau_2 \omega_p}{1 + \tau_2 \omega_p} \left[1 + \frac{\tau_4}{\tau_{24}} + \frac{\tau_1}{\tau_{21}} \right] \right)$$

$$= \frac{N_0}{1 + \tau_2 \omega_p} \left[1 + \tau_2 \omega_p \left(2 + \frac{\tau_4}{\tau_{24}} + \frac{\tau_1}{\tau_{21}} \right) \right]$$

$$\Delta N = N_2 - N_1 = N_2 \left(1 - \frac{\tau_1}{\tau_{21}} \right)$$

$$= N_0 \frac{\tau_2 \omega_p}{1 + \tau_2 \omega_p} \left(1 - \frac{\tau_1}{\tau_{21}} \right)$$

$$\Delta N = \frac{\tau_2 \omega_p (1 - \tau_1 / \tau_{21})}{1 + \tau_2 \omega_p (2 + \frac{\tau_4}{\tau_{24}} + \frac{\tau_1}{\tau_{21}})} N_c$$

3. Actually, this problem is trickier than I'd intended, because there are two fairly different solutions. I'll go through general procedure:

(5)

Know that at first mirror, $q = iz_0 = i \frac{\pi w_0^2}{\lambda}$.

To get beam at second mirror, use

$$M = \begin{bmatrix} 1 & 0 \\ \frac{2}{R} & 1 \end{bmatrix} \begin{bmatrix} 1 & d \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{bmatrix} \begin{bmatrix} 1 & d \\ 0 & 1 \end{bmatrix}$$

$$= \begin{bmatrix} 1 - \frac{d}{f} & 2d - \frac{d^2}{f} \\ \frac{2}{R} - \frac{1}{f} - \frac{2d}{Rf} & 1 + \frac{4d}{R} - \frac{d}{f} - \frac{2d^2}{Rf} \end{bmatrix}$$

So $q_{out} = \frac{A z_{in} + B}{C z_{in} + D} = \frac{A iz_0 + B}{C iz_0 + D} = iz_0$

Since want $q_{out} = iz_0$

Then $A iz_0 + B = -C z_0^2 + D iz_0$

$B + i(A-D)z_0 + C z_0^2 = 0$

Real + imaginary parts both zero:

$A = D$

$B + C z_0^2 = 0$

$A = D$ implies $1 - \frac{d}{f} = 1 - \frac{d}{f} + \frac{4df - 2d^2}{Rf}$

So $\frac{2df - d^2}{Rf} = 0$

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Actually two physically reasonable solutions:

i) $d = 2f$

ii) $R = \infty$

(Solution $d=0$ is not physical)

Consider (ii) first:

Still need $B + Cz_0^2 = 0$, with $R = \infty$, $B = 2d - \frac{d^2}{f}$
 $C = -\frac{1}{f}$

$$2d - \frac{d^2}{f} - \frac{z_0^2}{f} = 0$$

$$f = \frac{d^2 + z_0^2}{2d}$$

Stability: can just consider M since cavity is symmetric

Stable if $\left| \frac{A+D}{2} \right| \leq 1$

here $A = D = 1 - \frac{d}{f}$, so

$$\left| 1 - \frac{d}{f} \right| \leq 1$$

$$1 - \frac{d}{f} < 1 \quad \text{and} \quad 1 - \frac{d}{f} > -1$$

$$-\frac{d}{f} < 0 \quad \frac{d}{f} < 2$$

$$\Rightarrow f > 0 \quad f > \frac{d}{2}$$

But we have $f = \frac{d}{2} + \frac{z_0^2}{2d} > \frac{d}{2}$, so cavity is stable.

(7)

Now consider (1);

If $A = \frac{d}{z}$, then $B = 2d - 2d = 0$

$$C = \frac{z}{R} - \frac{z}{d} - \frac{4}{R} = -2\left(\frac{1}{R} + \frac{1}{d}\right)$$

Need

$$B + Cz_0^2 = 0$$

$$-2\left(\frac{1}{R} + \frac{1}{d}\right)z_0^2 = 0$$

$$\Rightarrow \boxed{R = -d} \quad (\text{independent of } z_0)$$

In this case,

$$A = -1$$

$$D = 1 + \frac{4d}{-d} - \frac{d}{d/2} - \frac{2d^2}{(-d)(d/2)}$$

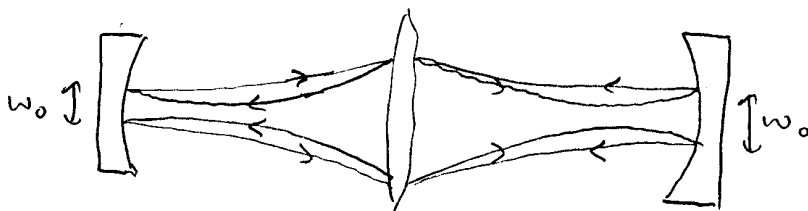
$$= 1 - 4 - 2 + 4 = -1$$

$$\text{So } \frac{A+D}{2} = -1, \quad \left| \frac{A+D}{2} \right| = 1$$

So cavity is marginally stable: stable, but right on the border.

That's why some cavity can support modes with different ω_0 's.

Note, this mode is not symmetric, looks like:



But it is a valid solution.

4. Basic principle is that for lasers to occur, have gain = loss. (8)

In one pass through medium, intensity is increased
by factor $G \equiv \frac{I(z=l)}{I(z=0)}$

and is decreased by factor $\frac{I_{\text{refl.out}}}{I_{\text{incident}}} = R = 1 - T$

So if I_- = intensity just before output coupler,
and I' = intensity after one round trip,

then $I' = G \times (1 - T) \times I$

In steady-state, $I' = I$, so $G = \frac{1}{1 - T}$

Our equation says $\ln \frac{I(l)}{I(0)} + \frac{I(l) - I(0)}{I_s} = \gamma_0 l$

$$\ln G + \frac{I(l)}{I_s} \left(1 - \frac{1}{G}\right) = \gamma_0 l$$

So solve for $I(l)$ = intensity exiting medium
= intensity incident on output coupler

$$I(l) = I_s \frac{1}{1 - \frac{1}{G}} [\gamma_0 l - \ln G]$$

$$\text{or } I(l) = I_s \frac{1}{1 - (1 - T)} [\gamma_0 l - \ln \frac{1}{1 - T}]$$

$$= I_s \frac{1}{T} [\gamma_0 l + \ln(1 - T)]$$

Then output intensity is $I_{\text{out}} = T I(l)$

$$I_{\text{out}} = I_s [\gamma_0 l + \ln(1 - T)]$$

Threshold when $I_{out} = 0$

or $\gamma_t = -\frac{1}{e} \ln(1-T)$

and output power $P = \pi \omega^2 I_{out}$

$$P = \pi \omega^2 I_s [\gamma_0 e - \ln(1-T)]$$

$$5. P_o = \pi w^2 I_s T \left(\frac{g_o}{T+L} - 1 \right)$$

If $g_o \gg T+L$, then

$$P_{out} = \pi w^2 I_s g_o \frac{T}{T+L}$$

$$\text{But } g_o = \frac{\lambda^2}{8\pi t_s \Delta\nu} \Delta N \quad \text{using } g(\nu) \approx \frac{1}{\Delta\nu}$$

$$\text{and } I_s = \frac{8\pi t_s h\nu}{\lambda^2 \tau_s} \Delta\nu_H \quad \text{homogeneous line width } \Delta\nu_H$$

$$\text{So } P_{out} = \pi w^2 \frac{h\nu}{\tau_s} \frac{\Delta\nu_H}{\Delta\nu} \Delta N \frac{T}{T+L}$$

$$\text{Also, } \Delta N = \frac{R(\tau_2 - \tau_1)}{1 + W_p \tau_2} \approx \frac{R \tau_2}{1 + W_p \tau_2}$$

$$\text{and } \tau_s = \frac{\tau_2}{1 + W_p \tau_2}$$

$$\text{So } P_{out} = \pi w^2 h\nu \frac{\Delta\nu_H}{\Delta\nu} R \frac{T}{T+L}$$

If $\Delta\nu + \Delta\nu_H$ don't depend on t_s , then

P_{out} is independent of t_s

Also, note $\nu = \frac{c}{\lambda}$, and $w \propto \sqrt{\lambda}$ in general.

So, P_{out} is also independent of λ

(11)

Note on beam waist:

At any point in cavity, mode parameter is

$$\frac{1}{q} = \frac{1}{B} \left[\frac{D-A}{2} \pm i \sqrt{1 - \left(\frac{A+D}{2}\right)^2} \right]$$

for $\begin{bmatrix} A & B \\ C & D \end{bmatrix}$ = round trip matrix starting from that point

So beam waist w at that point is given by

$$\frac{\lambda}{\pi w^2} = \text{Im} \frac{1}{q} = \pm \frac{1}{B} \sqrt{1 - \left(\frac{A+D}{2}\right)^2}$$

Note A, B, C, D are independent of λ .

So, have $\frac{\lambda}{w^2} = \text{constant}$

$$\boxed{w^2 \propto \lambda}$$